

THE KENYA NATIONAL EXAMINATIONS COUNCIL

# DIPLOMA IN BUILDING TECHNOLOGY DIPLOMA IN ARCHITECTURE 

MODULE III

## STRUCTURES III

3 hours

## INSTRUCTIONS TO CANDIDATES

You should have the following for this examination:
answer booklet;
scientific calculator:
This paper consists of EIGHT questions.
Answer any FIVE questions.
Maximum marks for each part of a question are as indicated.
All relevant tables for this examination are provided.
Candidates should answer the questions in English.

This paper consists of 14 printed pages.
Candidates should check the question paper to ascertain that all the pages are printed as indicated and that no questions are missing.

1. A 230 kN reaction from a beam of which a half is due to the imposed loads is supported at the top of a pin-jointed stanchion, 4 m long.
Check if a $203 \times 203 \times 46 \mathrm{~kg} / \mathrm{m}$ U.C. in grade S 275 steel is satisfactory.
Assume that the beam to stanchion connection is to the web as shown in figure 1.


Fig. 1


Using moment distribution method, analyse the loaded portal frame shown in figure 2 and hence draw the bending moment diagram showing values at critical points.


Fig. 2
3. A reinforced conerete suspended slab of a library is supported on universal beams as
shown in figure 3. The design loading has been estimated as:

- Dead loads from slab, finishes, self weight, etc $=6 \mathrm{kN} / \mathrm{m}^{2}$
- Imposed loads from furniture, books, etc $=4 \mathrm{kN} / \mathrm{m}^{2}$

Determine the suitable zection of universal beam for beam $B_{2}$ in grade $S 275$ stecl and hence check shear, moment capacity and deflection given that:

- permissible deflection $=1 /$ sen of span.
- $\mathrm{E}_{\text {vieel }}=210 \mathrm{kN} / \mathrm{mm}^{2}$
- Allowable shear $=0.6$ py
(20 marks)


Fig. 3
 Figure 4 shows a loaded continuous beam. Using the three moment theorem, analyze the beam and hence plot the shear force and bending moments diagram indicating values at critical points.
(20) marks)


Fig. 4
5. (a) State two methods of grading structural timber giving one advantage of each.
(b) Figure 5 shows a loaded timber joist beam. Check the adequacy of the $250 \times 100 \mathrm{~mm}$ joist in shear, bending and deflection given the following data:

Grade stresses for Cl 8 timber:

- In bending parallel to grain $=5.8 \mathrm{~N} / \mathrm{mm}^{2}$
- In shear parallel to grain $=0.67 \mathrm{~N} / \mathrm{mm}^{2}$

Permissible deffection $=1 / 360$ of span
Modification factors: $\mathrm{K}_{3}=1.25 \mathrm{~K}_{7}=1.04$ and $\mathrm{K}_{8}=1.1$
Actual deflection $\delta=\frac{5 u l^{+}}{384 E I}+\frac{\mathrm{WI}^{3}}{48 \mathrm{EI}}$
Where: $\mathrm{w}=$ imposed factored load (U.D.L.)
W = Imposed factored point loads.
$\mathrm{E}_{\text {mean }}=9100 \mathrm{~N} / \mathrm{mm}^{2}$
(16 marks)

6. (a) State three situations where influence lines can be applied in structures.
(b) A girder has a span of 40 m . Two concentrated loads of 18 kN and 25 kN at a fixed distance of 5 m , rolling along it are applied. Find the value of maximum B.M. and S.F. at $10 \mathrm{~m}, 20 \mathrm{~m}$ and 30 m from the left hand end.
7. Analyse the loaded beam shown in figure 6 using moment distribution method and hence draw the shear force and bending moment diagrams, indicating values at all critical points.
(20 marks)


Fig, 6
8. (a) Using neat sketches, illustrate the following types of welds:
(i) Double ' U' but weld;
(ii) Double 'V' butt weld;
(iii) Singlo ' J ' butt weld.
(b) Figure 7(a) shows a steel bolted joint of two tension members of size $15 \times 200 \mathrm{~mm}$

Determine suitable sizes of bolts to be used to withstand the tensile force applied of 175 kN .
Take: Shear strength of bolts $\mathrm{P}_{\mathrm{S}}=375 \mathrm{~N} / \mathrm{mm}^{2}$
Bearing strength on plate $P$ bt $=1000 \mathrm{~N} / \mathrm{mm}^{2}$


Fig. 7 (a)
(c) A single equal angle section of size $75 \times 75 \times 15 \mathrm{~mm}$ is welded to a gusset plate as shown in figure 7(b). It is to transmit a load of 160 kN . Design the joint using an 8 mm fillet weld given that:
permissible shear stress in weld $=220 \mathrm{~N} / \mathrm{mm}^{2}$.
(6 marks)


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Fig 7 (b)

Strength of bolts in clearance holes

|  | Bolt grade ( $\mathrm{N} / \mathrm{mm}^{2}$ ) |  |
| :--- | :--- | :---: |
|  | 4.6 | 8.8 |
| Shear strength, ph | 160 | 375 |
| Bearing, strength, B h | 460 | 1035 |
| Tension strength, P | 195 | 450 |

Strut table selection

| Type of section | Thickness ${ }^{\text {a }}$ | Axis of buckling |  |
| :---: | :---: | :---: | :---: |
|  |  | x-x | $y-y$ |
| Hot-rolled structural hollow section |  | - | - |
| Rolled I-section |  | - | - |
| Rolled H -section | Up to 40 mm | Table 8(a) | Table 8(b) |
|  | Over 40 mm | Table 8(b) | * |

${ }^{1}$ For thicknesses between 40 and 50 mm the value of po may be taken as the average of the values for thicknesses up to 40 mm and over 40 mm

| Areas of group of reinforcement bars ( $\mathrm{mm}^{2}$ ) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Buir } \\ \text { Diameter } \\ \text { (min) } \end{gathered}$ | Number of bars |  |  |  |  |  |  |  |  |  |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| 6 8 | 28 | 57 | 85 | 113 | 141 | 170 | 198 | 226 | 254 | 283 |
|  | 50 | 101 | 151 | 201 | 251 | 302 | 352 | 402 | 452 | 503 |
| 12 | $\begin{array}{r} 79 \\ 113 \end{array}$ | $\begin{aligned} & 157 \\ & 226 \end{aligned}$ | 236 339 | 314 | 393 565 | 471 679 | 550 | 628 | 707 | 785 |
| 16 | 201 | 402 | 603 | 804 | 1005 | 1206 | 1407 | 1608 | 1809 | 1131 |
| 20 | 314 | 628 | 942 | 1257 | 1571 | 1885 | 2199 | 2513 | 2827 | 3142 |
| 25 | 491 | 982 | 1473 | 1963 | 2454 | 2945 | 3436 | 3927 | 4418 | 4909 |
| 32 | 804 | 1608 | 2412 | 3216 | 4021 | 4825 | 5629 | 6433 | 7237 | 8042 |
| 40 | 1256 | 2513 | 3769 | 5026 | 6283 | 7539 | 8796 | 10050 | 11310 | 12570 |

UNIVERSAL BEAMS


DIMENSIONS

| Svetion Deaghtatur | Mass pary Metro <br> kgit： | Dupthor Seutior$\mathrm{n}$ | Wath 4 Sectian$\begin{gathered} \mathrm{B} \\ \mathrm{~mm} \end{gathered}$ | Thigrmm |  | Hoct Raghes$\stackrel{\mathrm{r}}{\mathrm{~mm}}$ | Onth Bopispert Fively <br> d ms | Batias for Lops Bucking |  | Dimensiong fir Dosailing |  |  | Gramin Arsy |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | WatI |  |  |  | $\begin{aligned} & \text { Flangn } \\ & \text { brt } \end{aligned}$ | Whed ， 4 |  | Nonh |  |  |  |
|  |  |  |  | $\frac{1}{m}$ | $\stackrel{T}{\mathrm{~m}}$ |  |  |  |  |  | $\mathrm{M}$ | $\frac{\pi}{n}$ |  |  |
| $407 \times 191 \times 36$ $407 \times 127 \times 199$ $457 \times 191 \times 98$ $45 x^{2} 16 \pi x$ $45 \text { र हा } 191 \times 6$ | $\begin{array}{r} 20.3 \\ 50.3 \\ 20.0 \\ 74.3 \\ 68.1 \end{array}$ | 2072 6194 4600 460 4534 |  | 11.4 10.5 8.9 90 8.5 | 180 187 110 145 127 | $\begin{aligned} & 16.2 \\ & 102 \\ & 102 \\ & 102 \\ & 102 \end{aligned}$ | $\begin{aligned} & 407.8 \\ & 407.3 \\ & 407.3 \\ & 407 / \\ & 407 . \end{aligned}$ | $\begin{aligned} & 492 \\ & 580 \\ & 5.08 \\ & 6.97 \\ & 7.818 \end{aligned}$ | 35.8 94.8 41.2 45.3 40.0 | $\begin{aligned} & \frac{8}{7} \\ & \frac{1}{7} \\ & \frac{1}{2} \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \\ & 109 \\ & 102 \\ & 102 \end{aligned}$ | $\begin{aligned} & 30 \\ & 38 \\ & 20 \\ & \frac{k 0}{24} \\ & \frac{1}{24} \end{aligned}$ | $\begin{aligned} & 1.07 \\ & 1.86 \\ & 1.85 \\ & 1.64 \\ & 1.89 \end{aligned}$ | $\begin{aligned} & 159 \\ & 159 \\ & 20.1 \\ & 20.1 \\ & 243 \end{aligned}$ |
|  | 307 742 372 35.2 52.3 | 655.8 <br> 6820 <br> 458.0 <br> 4546 <br> 4028 | 155.3 154.4 15.9 1529 152.4 | 10.5 9.6 9.0 618 78 | 12.9 170 15.0 13.3 109 | $\begin{aligned} & 102 \\ & 102 \\ & 102 \\ & \hline 102 \\ & 102 \end{aligned}$ | 40 <br> 400.8 <br> tor： 8 <br> 4015 <br> 400.5 | 8.11 <br> 454 <br> stb <br> 3.15 <br> flent | $\begin{aligned} & 38.8 \\ & 48.5 \\ & 453 \\ & 30.3 \\ & 39.1 \end{aligned}$ | $\begin{aligned} & \frac{7}{2} \\ & \frac{1}{6} \\ & \frac{1}{6} \end{aligned}$ | $\begin{aligned} & 94 \\ & 04 \\ & 34 \\ & 84 \\ & 84 \end{aligned}$ | $\begin{aligned} & \frac{30}{20} \\ & \frac{20}{20} \\ & \frac{21}{20} \end{aligned}$ | $\begin{aligned} & 1.91 \\ & 1.90 \\ & 150 \\ & 1.49 \\ & 148 \end{aligned}$ | $\begin{aligned} & 184 \\ & 80.3 \\ & 22.3 \\ & 34.9 \\ & 38.2 \end{aligned}$ |
| $\begin{aligned} & 406 \times 173=74 \\ & 460 \times 173 \times 87 \\ & 400 \times 173 \times 80 \\ & 405 \times 178 \times-54 \end{aligned}$ | $\begin{aligned} & 74.2 .1 \\ & 37.1 \\ & 20.1 \\ & 54.1 . \end{aligned}$ | 412.8 40.4 400.4 40208 | $\begin{aligned} & 170.5 \\ & \text { 178 } \\ & 1769 \\ & 177.7 \end{aligned}$ | 9.5 0.8 7.8 7.7 | $\begin{aligned} & 10.9 \\ & 14.3 \\ & 12.3 \\ & 10.2 \end{aligned}$ | $\begin{aligned} & 102 \\ & 162 \\ & 302 \\ & 102 \end{aligned}$ | $\begin{aligned} & 300.4 \\ & 360.4 \\ & 380.4 \\ & 760.4 \end{aligned}$ | $\begin{aligned} & 5191 \\ & \text { fin } \\ & 535 \\ & 535 \end{aligned}$ | $\begin{aligned} & 129 \\ & 41.0 \\ & 15.0 \\ & 16.8 \end{aligned}$ | $\begin{aligned} & f \\ & 6 \\ & \frac{1}{6} \end{aligned}$ | $\begin{aligned} & 180 \\ & 95 \\ & 96 \\ & 96 \end{aligned}$ | $\begin{aligned} & 20 \\ & 26 \\ & 24 \\ & 24 \\ & 22 \end{aligned}$ | $\begin{aligned} & 1.51 \\ & 1.50 \\ & 1.69 \\ & 1.48 \end{aligned}$ | $\begin{aligned} & 203 \\ & 208 \\ & 248 \\ & 27 A \end{aligned}$ |
| $406 \times 149 \times 48$ $+06 \times 140 \times 19$ | 280 300 | 408.2 350.0 | 1427 1418 | $\begin{aligned} & 6.0 \\ & 84 \end{aligned}$ | 11.2 <br> 8.6 | $\begin{array}{r} 102 \\ 102 \end{array}$ | 2604， | $\begin{aligned} & 8.36 \\ & 84 \end{aligned}$ | $\begin{aligned} & 390 \\ & 5013 \end{aligned}$ | $5$ | $\begin{aligned} & 38 \\ & 78 \end{aligned}$ | $\begin{aligned} & 22 \\ & 30 \end{aligned}$ | $\begin{array}{r} 134 \\ +193 \end{array}$ | $\begin{array}{r} 22 \\ 92 \\ \hline \end{array}$ |
| $\begin{aligned} & 308 \times 171 \times 9 \mathrm{Cl} \\ & 309 \times 171 \times 57 \\ & 358 \times 171 \times 51 \\ & 356 \times 171 \times 48 \end{aligned}$ | $\begin{aligned} & \operatorname{tr1} \\ & 470 \\ & 310 \\ & 450 \end{aligned}$ | $\begin{aligned} & 3 m 24 \\ & 15 t 0 \\ & 3020 \\ & 351.4 \end{aligned}$ | 1732 1722 17.5 121.1 | 8.1 8.1 7.4 7.0 | $\begin{aligned} & 15.2 \\ & 13.0 \\ & 113 \\ & 97 \end{aligned}$ | $\begin{aligned} & 102 \\ & 102 \\ & 102 \\ & 102 \end{aligned}$ | $\begin{aligned} & 318 \\ & 318 \\ & 3118 \\ & 31,5 \end{aligned}$ | 5.52 <br> K荡 <br> 7． 6 <br> \＃12 | $\begin{aligned} & 342 \\ & 3 e 5 \\ & 121 \\ & 445 \end{aligned}$ | $\begin{aligned} & 7 \\ & \frac{9}{5} \\ & \frac{1}{8} \end{aligned}$ | $\begin{aligned} & 94 \\ & 94 \\ & 04 \\ & 94 \end{aligned}$ | $\begin{aligned} & 24 \\ & 24 \\ & 20 \\ & 80 \end{aligned}$ | $\begin{aligned} & 1,99 \\ & 1.97 \\ & 1.38 \\ & 1.07 \end{aligned}$ | $\begin{aligned} & 2 m n \\ & 241 \\ & 347 \\ & 301 \end{aligned}$ |
| $356 \sim 127 \times 30$ $756 \times 127 \times 29$ | 39.7 20.7 | 3814 3820 | 1850 124.4 | $\begin{aligned} & 6.6 \\ & e .0 \end{aligned}$ | $\begin{aligned} & 30.7 \\ & 6.5 \end{aligned}$ | $\begin{aligned} & 102 \\ & 102 \end{aligned}$ | $\begin{aligned} & \text { य11 } \\ & 321.6 \end{aligned}$ | $\begin{aligned} & \text { 518 } \\ & 738 \end{aligned}$ | $\begin{aligned} & 472 \\ & 51.9 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \end{aligned}$ | $\frac{\pi}{\pi}$ | $\frac{20}{2 a}$ | 1.818 1.17 | 3038 |
| $\begin{aligned} & 305 \times 106 \times 54 \\ & 305 \times 105 \times 14 \\ & 305 \times 105=10 \\ & \hline \end{aligned}$ | $\begin{aligned} & 540 \\ & 25.1 \\ & 40.3 \end{aligned}$ | $\begin{aligned} & 3104 \\ & 308,{ }_{2}^{1} \\ & 300.4 \end{aligned}$ | $\begin{array}{r} 1889 \\ 1057 \\ +85: 0 \end{array}$ | $\begin{aligned} & 70 \\ & 87 \\ & 0.0 \end{aligned}$ | $\begin{aligned} & 13 y \\ & 14,18 \\ & 108 \end{aligned}$ | $\begin{aligned} & 89 \\ & 69 \\ & 89 \end{aligned}$ | $\begin{aligned} & 2659 \\ & 2552 \\ & 2652 \end{aligned}$ | $\begin{aligned} & 8.00 \\ & 7.00 \\ & -8.6 p \end{aligned}$ | $\begin{aligned} & 39.21 \\ & 30.6 \\ & 462 \end{aligned}$ | $\frac{8}{5}$ | $\begin{aligned} & 90 \\ & 30 \\ & 90 \end{aligned}$ |  | $\begin{aligned} & 125 \\ & 125 \\ & 124 \end{aligned}$ | $\begin{aligned} & 233 \\ & \text { 201 } \\ & \text { soal } \end{aligned}$ |
| $\begin{aligned} & 305 \times 127 \times 4 n \\ & 20 f \times 127=12 \\ & 305 \times 127 \times 37 \end{aligned}$ | $\begin{aligned} & 43,1 \\ & 419 \\ & 3 \geq 0 \end{aligned}$ | $\begin{array}{r} 3+1.0 . \\ 307.2 \\ -304.4 \end{array}$ | $\begin{aligned} & 132 \\ & 1243 \\ & 1224 \end{aligned}$ | $\begin{aligned} & 80 \\ & 30 \\ & 20 \end{aligned}$ | $\begin{aligned} & 940 \\ & 13, \\ & 10.7 \end{aligned}$ | $\begin{aligned} & 3.9 \\ & 3.8 \\ & 3.0 \end{aligned}$ | $\begin{aligned} & 2882 \\ & 2952 \\ & 2858 \end{aligned}$ | $\begin{aligned} & 44 y \\ & \text { E14 } \\ & 5 \pi 7 \end{aligned}$ |  | $\begin{aligned} & 7 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 00 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 3 t \\ & 32 \\ & 30 \end{aligned}$ | $\begin{aligned} & 1.09 \\ & 100 \mathrm{OE} \\ & \mathrm{t} 0 \mathrm{~F} \end{aligned}$ | $\begin{aligned} & 2877 \\ & 25.8 \\ & 2909 \end{aligned}$ |
| $\begin{aligned} & 305 \times 102=00 \\ & 305 \times 102 \times 20 \\ & 365 \times 162 \times 25 \end{aligned}$ | $\begin{aligned} & 38.9 \\ & \frac{38.2}{24.3} \end{aligned}$ | $\begin{aligned} & 252.27 \\ & 3687 \\ & 315.1 \end{aligned}$ | $\begin{aligned} & \text { ytay } \\ & \text { yata } \\ & \text { tas. } \end{aligned}$ | $\begin{aligned} & 5.8 \\ & 6.0 \\ & 8.9 \end{aligned}$ | $\begin{aligned} & 108 \\ & 5.8 \\ & 7.0 \end{aligned}$ | $\begin{aligned} & 7.6 \\ & 7.8 \\ & 76 \end{aligned}$ | $\begin{aligned} & 2750 \\ & \text { apto } \\ & \text { athoi } \end{aligned}$ | $\begin{aligned} & 4.74 \\ & 125 \\ & 728 \end{aligned}$ | $\begin{aligned} & 4128 \\ & 4608 \\ & 475 \end{aligned}$ | $\begin{aligned} & 8 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & \text { GR } \\ & 00 \\ & 58 \end{aligned}$ | $\begin{gathered} 20 \\ 70 \\ 70 \\ 70 \end{gathered}$ | $\begin{aligned} & 1.09 \\ & 1.00 \\ & 0.008 \end{aligned}$ | $\begin{gathered} 301 \\ 350 \\ 4) 0 \end{gathered}$ |
| $\begin{aligned} & 254 \times 148 \times 34 \\ & 25 \times 148 \times 3 \\ & 25 \times 14 \times 3 t \end{aligned}$ | $\begin{aligned} & 430 \\ & 370 \\ & 310 \end{aligned}$ | $\begin{aligned} & 252.6 \\ & 9560 \\ & 2520 \end{aligned}$ |  | $\begin{aligned} & 2.2 \\ & 6.3 \\ & 8.0 \end{aligned}$ | $\begin{aligned} & 12.7 \\ & 309 \\ & 3.9 \end{aligned}$ | 78 78 785 | $\begin{aligned} & 2139 \\ & 2139 \\ & 2190 \end{aligned}$ | $\begin{aligned} & 306 \\ & 8.02 \\ & 8.67 \end{aligned}$ | $\begin{aligned} & 30.6 \\ & 36 \cdot \mathrm{e} \\ & 3 \mathrm{~F} .5 \end{aligned}$ | $\begin{aligned} & \frac{5}{5} \\ & 5 \end{aligned}$ | $\begin{aligned} & 8 e \\ & \frac{30}{3} \end{aligned}$ | $\frac{22}{18}$ | $\begin{aligned} & 1.08 \\ & 107 \\ & 108 \\ & 108 \end{aligned}$ | $\begin{aligned} & 251 \\ & 301 \\ & 362 \end{aligned}$ |
| $\begin{aligned} & 354 \times 102 \times 30 \\ & 254 \times 102 \times 28 \\ & 254 \times 108=25 \end{aligned}$ | $\begin{aligned} & 39.3 \\ & 2 \& 2 \\ & 20.0 \end{aligned}$ |  | $\begin{aligned} & 100= \\ & 100.3 \\ & 1014 \end{aligned}$ | $\begin{aligned} & 69 \\ & 60 \\ & 57 \end{aligned}$ | $\begin{aligned} & 100.1 \\ & \text { i. } \\ & \mathbf{~} .0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 78 \\ & 78 \\ & 70 \\ & 7.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 205 ? \\ & 2262 \\ & 22512 \end{aligned}$ | $\begin{aligned} & 511 \\ & 60 \% \\ & 7.47 \end{aligned}$ | $\begin{aligned} & 357 \\ & 35.7 \\ & 30.7 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \\ & \hline \end{aligned}$ |  | $\begin{gathered} 18 \\ 16 \\ 16 \end{gathered}$ | $\begin{aligned} & 1804 \\ & \text { 2as9 } \\ & \text { caso } \end{aligned}$ | $\begin{aligned} & 32.9 \\ & 74.6 \\ & 4.5 \end{aligned}$ |
|  | $\begin{aligned} & 3010 \\ & 251 \end{aligned}$ | $\begin{aligned} & \text { Poca } \\ & \text { axiz } \end{aligned}$ | $\begin{array}{r} 4339 \\ 1338 \end{array}$ | $\frac{64}{14}$ | $\frac{04}{1 \mathrm{~A}}$ | $\begin{aligned} & 18 \\ & 18 \end{aligned}$ | $\begin{aligned} & 1 / 24 \\ & 17<4 \end{aligned}$ | $\begin{aligned} & 6.95 \\ & 8.54 \end{aligned}$ | $\frac{2939}{302}$ | $\frac{5}{4}$ | $\begin{aligned} & 74 \\ & 14 \end{aligned}$ | $\begin{aligned} & 1 \pi \\ & 90 \\ & \hline 9 \end{aligned}$ | $\begin{aligned} & \text { onen } \\ & \text { in\# } \end{aligned}$ | $\begin{aligned} & 30.1 \\ & 32.1 \end{aligned}$ |
| 205 以 Cim | 83， 7 | 7ay | 1014 | 5.4 | ＊23 | 780 | 162． 4 | 547 | 21．4 | 5 | 0 | 10 | 0.790 | 34.8 |
| 178x $108 \times 18$ | 180 | 177.1 | 1912 | ¢ 8 | 72 | $17 \%$ | 445： | A 41 | 30．63 | 4 | 60 | 409 | 0.738 | tin 5 |
| 4120303016 | 18.9 | 1524 | 甠圌 | 4.5 | 17 | 78 | 122.8 | Sive | 27.1 | 4 | 58 | 16 | C6sal | 308 |
| $127 \times 75=15$ | 118 | －187，0 | 780 | 40 | 28 | 78 | 30.0 | 5.9018 | \％ 4. | 4 | elin 4 | 17 | 4537 | $4 \div 3$ |

Table 8(a): Compressive strength, $p_{c}\left(\mathrm{~N} / \mathrm{mm}^{2}\right)$ for struts

| $\lambda_{\lambda} P y$ | 225 | 245 | 255 | 265 | 275 | $\int_{2}{ }^{P y}$ | 225 | 245 | 255 | 265 | 275 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 225 | 245 | 255 | 265 | 275 | 96 | 133 | 140 | 143 | 146 | 148 |
| 20 | 224 | 243 | 253 | 263 | 272 | 98 | 130 | 137 | 139 | 142 | 245 |
| 25 | 220 | 239 | 248 | 258 | 267 | 100 | 127 | 133 | 136 | 138 | 141 |
| 30 | 216 | 234 | 243 | 253 | 262 | 102 | 124 | 130 | 132 | 135 | 137 |
| 35 | 211 | 229 | 238 | 247 | 256 | 104 | 122 | 127 | 129 | 131 | 133 |
| 40 | 207 | 224 | 233 | 241 | 250 | 106 | 119 | 124 | 126 | 128 | 230 |
| 42 | 205 | 222 | 231 | 239 | 248 | 108 | 116 | 121 | 123 | 125 | 126 |
| 44 | 203 | 220 | 228 | 237 | 245 | 110 | 113 | 118 | 120 | 121 | 123 |
| 46 | 201 | 218 | 226 | 234 | 242 | 112 | 111 | 115 | 117 | 118 | 120 |
| 48 | 199 | 215 | 223 | 231 | 239 | 114 | 108 | 112 | 114 | 115 | 117 |
| 50 | 197 | 213 | 221 | 229 | 297 | 116 | 105 | 109 | 111 | 112 | 114 |
| 52 | 195 | 210 | 218 | 226 | 234 | 118 | 103 | 106 | 108 | 109 | 111 |
| 54 | 192 | 208 | 215 | 223 | 230 | 120 | 100 | 104 | 105 | 107 | 108 |
| 56 | 190 | 205 | 213 | 220 | 227 | 122 | 98 | 101 | 103 | 104 | 105 |
| 58 | 188 | 202 | 210 | 217 | 224 | 124 | 96 | 99 | 100 | 101 | 102 |
| 60 | 185 | 200 | 207 | 214 | 221 | 126 | 94 | 96 | 97 | 99 | 100 |
| 62 | 183 | 197 | 204 | 210 | 227 | 128 | 91 | 94 | 95 | 96 | 97 |
| 54 | 180 | 194 | 200 | 207 | 213 | 130 | 89 | 92 | 93 | 94 | 95 |
| 66 | 178 | 191 | 197 | 203 | 210 | 135 | 84 | 86 | 87 | B8 | 89 |
| 68 | 175 | 188 | 194 | 200 | 206 | 140 | 79 | 81 | 82 | 83 | 84 |
| 70 | 172 | 185 | 190 | 196 | 202 | 145 | 75 | 77 | 78 | 78 | 79 |
| 72 | 169 | 181 | 187 | 193 | 198 | 150 | 71 | 72 | 73 | 74 | 74 |
| 74 | 167 | 178 | 183 | 189 | 194 | 155 | 61 | 69 | 69 | 70 | 70 |
| 76 | 164 | 175 | 180 | 185 | 190 | 160 | 64 | 65 | 66 | 66 | 66 |
| 78 | 161 | 171 | 176 | 181 | 186 | 165 | 60 | 61 | 62 | 63 | 63 |
| 80 | 158 | 168 | 172 | 177 | 181 | 170 | 57 | 58 | 59 | 59 | 60 |
| 82 | 255 | 164 | 169 | 173 | 177 | 175 | 55 | 56 | 56 | 56 | 57 |
| 84 | 152 | 161 | 165 | 169 | 173 | 180 | 52 | 53 | 53 | 54 | 54 |
| 85 | 149 | 157 | 161 | 165 | 169 | 185 | 49 | 50 | 51 | 51 | 51 |
| 88 | 146 | 154 | 158 | 161 | 165 | 190 | 47 | 48 | 48 | 48 | 49 |
| 90 | 143 | 150 | 154 | 157 | 161 | 195 | 45 | 46 | 46 | 46 | 47 |
| 92 | 139 | 147 | 150 | 153 | 156 | 200 | 43 | 44 | 44 | 44 | 44 |
| 94 | 136 | 143 | 147 | 150 | 152 |  |  |  |  |  |  |

Table $\mathrm{a}(\mathrm{b})$ : Compressive strength, $\mathrm{Pc}_{\mathrm{c}}\left(\mathrm{N} / \mathrm{mm}^{2}\right)$ for struts

| $\boldsymbol{P Y}$ | 225 | 245 | 255 | 265 | 275 | $p y$ | 225 | 245 | 255 | 265 | 275 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15 | 225 | 245 | 255 | 265 | 275 | 96 | 118 | 124 | 127 | 129 | 132 |
| 20 | 224 | 242 | 252 | 261 | 271 | 98 | 115 | 121 | 123 | 126 | 129 |
| 25 | 217 | 235 | 245 | 254 | 263 | 100 | 112 | 118 | 120 | 123 | 125 |
| 30 | 211 | 228 | 237 | 246 | 255 | 102 | 110 | 115 | 118 | 120 | 122 |
| 35 | 204 | 221 | 230 | 238 | 247 | 104 | 107 | 112 | 115 | 117 | 119 |
| 40 | 198 | 214 | 222 | 230 | 238 | 106 | 105 | 110 | 112 | 114 | 116 |
| 42 | 195 | 211 | 219 | 227 | 235 | 108 | 102 | 107 | 109 | 111 | 113 |
| 44 | 193 | 208 | 216 | 224 | 231 | 110 | 100 | 104 | 106 | 108 | 110 |
| 46 | 190 | 205 | 213 | 220 | 228 | 112 | 98 | 102 | 104 | 106 | 107 |
| 48 | 187 | 202 | 209 | 217 | 224 | 114 | 96 | 99 | 101 | 103 | 105 |
| 50 | 184 | 199 | 206 | 213 | 220 | 116 | 93 | 97 | 99 | 101 | 102 |
| 52 | 181 | 196 | 203 | 210 | 217 | 118 | 91 | 95 | 96 | 98 | 100 |
| 54 | 179 | 193 | 199 | 206 | 213 | 120 | 89 | 93 | 94 | 96 | 97 |
| 56 | 176 | 189 | 196 | 202 | 209 | 122 | 87 | 91 | 92 | 93 | 95 |
| 58 | 173 | 186 | 192 | 199 | 205 | 124 | 85 | 88 | 90 | 91 | 92 |
| 60 | 170 | 183 | 189 | 195 | 201 | 126 | 83 | 86 | 88 | 89 | 90 |
| 62 | 167 | 179 | 185 | 191 | 197 | 128 | 82 | 84 | 86 | 87 | 88 |
| 64 | 164 | 176 | 182 | 188 | 193 | 130 | 80 | 82 | 84 | 85 | 86 |
| 66 | 161 | 173 | 178 | 184 | 189 | 135 | 75 | 78 | 79 | 80 | 81 |
| 68 | 158 | 169 | 175 | 180 | 185 | 140 | 71 | 74 | 75 | 76 | 76 |
| 70 | 155 | 166 | 171 | 176 | 181 | 145 | 68 | 70 | 70 | 71 | 72 |
| 72 | 152 | 163 | 168 | 172 | 177 | 150 | 64 | 66 | 67 | 68 | 68 |
| 74 | 149 | 159 | 164 | 169 | 173 | 155 | 61 | 63 | 83 | 64 | 65 |
| 76 | 146 | 156 | 160 | 165 | 169 | 160 | 58 | 59 | 60 | 61 | 61 |
| 78 | 143 | 152 | 157 | 161 | 165 | 165 | 55 | 56 | 57 | 58 | 58 |
| 80 | 140 | 149 | 153 | 157 | 161 | 170 | 52 | 54 | 54 | 55 | 55 |
| 82 | 137 | 146 | 150 | 154 | 157 | 175 | 50 | 51 | 52 | 52 | 53 |
| 84 | 134 | 142 | 146 | 150 | 154 | 180 | 48 | 49 | 49 | 50 | 50 |
| 86 | 132 | 139 | 143 | 146 | 150 | 185 | 46 | 46 | 47 | 47 | 48 |
| 88 | 129 | 136 | 139 | 143 | 146 | 190 | 43 | 44 | 45 | 45 | 46 |
| 90 | 126 | 133 | 136 | 139 | 142 | 195 | 42 | 42 | 43 | 43 | 43 |
| 92 | 123 | 130 | 133 | 136 | 139 | 200 | 40 | 41 | 41 | 41 | 42 |
| 94 | 120 | 127 | 130 | 133 | 135 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

## UNIVERSAL COLUMINS



PROPERTIES

| BNetion Daspogaion | Bucond Namarsof thome If Now |  | Haxlun of Eyration |  | Amitr <br> Modula |  | Thate Modvain |  | Buciding Farmollor <br> 11 | Jormionai Inctax <br> $\pi$ | Waperer Corntyr <br> H © $4 \mathrm{~F}^{\circ}$ | Tarcignal Combant$\frac{1}{2 m}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { foon } \\ & x=1 \\ & \text { for } \end{aligned}$ | Axin <br> FH | $\begin{aligned} & \text { Noty } \\ & \text { pix } \\ & \text { ant } \end{aligned}$ |  | Axay <br> XCX <br> （17 ${ }^{2}$ | $\left\lvert\, \begin{aligned} & A x s \\ & \mathrm{~cm}^{3} \end{aligned}\right.$ | An $x \times$ $o n^{2}$ | $\begin{aligned} & \mathrm{arlz} \\ & \mathrm{H} \\ & \mathrm{~min} \end{aligned}$ |  |  |  |  |  |
|  | 276000 <br> 229000 <br> 185000 <br> 147000 <br> 125800 <br> 89600 <br> ग7loc |  | 184 <br> 180 <br> 178 <br> $17 \%$ <br> 169 <br> 189 <br> 189 | 110 100 10.7 70.5 10.4 10.2 102 |  |  | $\begin{aligned} & 18200 \\ & 12400 \\ & 10000 \\ & k 220 \\ & 7000 \\ & 1000 \\ & 4800 \end{aligned}$ | 710 <br> 6000 <br> 18000 <br> 450 <br> 3340 <br> 1980 <br> 2380 | $\begin{aligned} & 0.343 \\ & 0.841 \\ & 0.909 \\ & 0.497 \\ & 0.335 \\ & 0.554 \\ & 6.835 \end{aligned}$ | 5.46 8.05 6.80 7.97 3.84 102 12.0 | $\begin{aligned} & 38.8 \\ & 34.1 \\ & 24.3 \\ & 180 \\ & 15.0 \\ & 123 \\ & 9.54 \\ & \hline \end{aligned}$ | 43508 9540 <br> 5 Tsma <br> 290 <br> 140 <br> t12 |  |
|  |  | $\begin{aligned} & 2700 \\ & 21500 \\ & 12500 \\ & 1+600 \end{aligned}$ | $\begin{aligned} & 10.7 \\ & 18.9 \\ & 15.8 \\ & \text { fils } \end{aligned}$ | $\begin{aligned} & 8.80 \\ & 9.51 \\ & \hline 0.69 \\ & 8.49 \end{aligned}$ | $\begin{aligned} & 2540 \\ & 3100 \\ & 0690 \\ & 2700 \end{aligned}$ | 1200 1150 940 283 | $\begin{aligned} & 2970 \\ & 3460 \\ & 2979 \\ & 2610 \end{aligned}$ | $\begin{aligned} & 1806 \\ & 1600 \\ & 1400 \\ & 1000 \end{aligned}$ | 6.844 <br> 0.382 <br> 0.864 <br> あぁた | $\begin{aligned} & 13.4 \\ & 16.0 \\ & 17.0 \\ & 12.0 \end{aligned}$ | 7.14 <br> 0.00 <br> E． 11 <br> 4.5 블 |  | 28 <br> 295 <br> 35 <br> 104 |
| $\begin{aligned} & 305 \times 305 \times 201 \\ & 305 \times 306 \times 240 \\ & 305 \times 305 \times 190 \\ & 395 \times 305 \approx=750 \\ & 305 \times 300=191 \\ & 305 \times 305 \times 118 \\ & 305=306 \times 39 \end{aligned}$ | 70000 8800 30000 30500 20300 27200 82900 | 20000 <br> 20000 <br> 78500 <br> 18000 <br> 10700 <br> 7080 <br> 7310 | 14.3 14.5 <br> 14.2 13 19.7 150 13.4 | $\begin{aligned} & 8.27 \\ & 0.15 \\ & 8.04 \\ & 7.00 \\ & 7.83 \\ & 7.78 \\ & 7.82 \end{aligned}$ | $\begin{aligned} & 4390 \\ & 3840 \\ & 3000 \\ & 2370 \\ & 3090 \\ & 1760 \\ & 1450 \end{aligned}$ | 1530 <br> 1200 <br> 1020 <br> 308 <br> 692 <br> 589 <br> 472 | $\begin{aligned} & 5110 \\ & 4850 \\ & 3440 \\ & 2510 \\ & 2000 \\ & 1060 \\ & 1500 \end{aligned}$ | 2240 $\pm 950$ 1620 1250 1050 925 728 | 2058 <br> Qass <br> $0=4$ <br> － 0.302 <br> 0.85 <br> 16.82 | $\begin{aligned} & 7.85 \\ & 7.74 \\ & 10.2 \\ & 725 \\ & 14.1 \\ & 162 \\ & 10.2 \end{aligned}$ | 530 5.01 3.89 2.87 1.30 1.88 1.85 | 2000 4270 734 330 249 101 34.2 | $\begin{aligned} & 365 \\ & 306 \\ & 202 \\ & 271 \\ & i 24 \\ & 130 \\ & 123 \end{aligned}$ |
| $\begin{aligned} & 254 \times 254 \times 197 \\ & 254 \times 254 \times 1.20 \\ & 254 \times 244 \times 10 \\ & 254 \times 254 \times 19 \\ & 254 \times 254 \times 72 \end{aligned}$ |  |  | $\begin{aligned} & 18.7 \\ & 11.8 \\ & 11.12 \\ & 11.2 \\ & 11.1 \end{aligned}$ | $\begin{aligned} & 5.81 \\ & 6.09 \\ & 0.59 \\ & 8.55 \\ & 0.48 \end{aligned}$ | $\begin{aligned} & 2980 \\ & 1630 \\ & 1810 \\ & 1100 \\ & 190 \end{aligned}$ | $\begin{aligned} & 746 \\ & 576 \\ & 4501 \\ & 379 \\ & 307 \end{aligned}$ | $\begin{aligned} & 2400 \\ & 1070 \\ & 3450 \\ & 1220 \\ & 392 \end{aligned}$ | 1720 375 677 575 465 | 0.851 0.850 0.849 8.851 0.849 | $\begin{aligned} & 8.50 \\ & 103 \\ & 124 \\ & 14.5 \\ & 179 \end{aligned}$ | $\begin{aligned} & 1.83 \\ & +10 \\ & 0.198 \\ & \text { a.75 } \\ & 4.5 e 8 \end{aligned}$ | CRE <br> 212 <br> 172 <br> 109 <br> 573 | $\begin{aligned} & 123 \\ & \hline 274 \\ & 189 \\ & 130 \\ & 113 \\ & 32.1 \end{aligned}$ |
|  |  | 1130 2540 2090 1780 1650 |  | $\begin{aligned} & 534 \\ & 8,90 \\ & 3.20 \\ & 518 \\ & 5,15 \end{aligned}$ | 350 $700^{-}$ 534 510 450 | $\begin{aligned} & 299 \\ & 296 \\ & 201 \\ & 174 \\ & 102 \end{aligned}$ | $\begin{aligned} & 977 \\ & 794 \\ & 650 \\ & 367 \\ & 48 \end{aligned}$ | $\begin{aligned} & 439 \\ & 374 \\ & 305 \\ & 2041 \\ & 231 \end{aligned}$ |  | $\begin{aligned} & 102 \\ & 11.9 \\ & 14.1 \\ & 15.8 \\ & 12.7 \end{aligned}$ | $\begin{aligned} & 0.313 \\ & 0.250 \\ & 0.197 \\ & 0.167 \\ & 0.1420 \end{aligned}$ | $\begin{array}{r} 198 \\ 809 \\ 472 \\ 218 \\ 228 \end{array}$ |  |
| $\begin{aligned} & 352 \times 152 \times 37 \\ & 159 \times 152 \times 30 \\ & 152 \times 152=22 \end{aligned}$ | $\begin{aligned} & \mathrm{nero} \\ & 1700 \\ & 1250 \end{aligned}$ | 706 0 <br> 500 6 <br> 400 6 | $\begin{array}{l\|l} 6 \pi & 3 \\ 678 & 2 \\ 6[14 & 1 \end{array}$ | $\begin{aligned} & 383 \\ & \begin{array}{l} 183 \\ 1 \end{array} \end{aligned}$ | $\begin{array}{l\|l} 273 & 3 \\ 202 & 3 \\ f B 4 & = \end{array}$ | 31.5  <br> 73.3  <br> 7.5  |  | $\begin{aligned} & 146 \\ & 102 \\ & 062 \end{aligned}$ | $\$ 849$ 0348 0840 | 1333  <br> 180  <br> 20.7 0 | $\begin{aligned} & a .0099 \\ & \text { a.0501 } \\ & 0.027 ? \end{aligned}$ | 192 195 483 | 48．1 <br> $38:$ <br> 29.2 |

## UNIVERSAL COLUMNS



DIMENSIONS

| Spation Designation |  |  | Wath of Sexthin <br> 4 min | Thictoress |  | Ahot Ructus | Deph Duthsan 7lysa$3 \mathrm{~m}$ | Fisjan lar Lioal Buiding |  | Dinemsons fur Deveing |  |  | Surtus Ama |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Whe <br> It tim |  |  |  | $\begin{array}{\|l\|} \hline \text { Fixnge } \\ \text { BT } \end{array}$ | $\begin{aligned} & \text { Weo } \\ & d t \end{aligned}$ | firt Cxamenon C Tा | Nath |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | $\frac{n}{n}$ | $\left\|\begin{array}{c} n \\ \mathrm{ma} \end{array}\right\|$ |  |  |
| 35ex $\times 468 \times-64$ | 6510 | 474.6 | 454.0 | 47.8 | 72.0 | 152 | 2902 | 2.75 | 10.0 | \％ | 100 | 5 | 253 | 3.38 |
| 15e r $405 \times 15 \%$ ， | 551.0 | 445.0 | 418．5 | 42.1 | 07.5 | 152 | 2002 | 2,10 | L． 30 | 2 | 200 | 04 | 248 | 449 |
|  | 487.0 | 48.4 | 412－2 | \＄50． | 80.0 | 158 | 2902 | 750 | L21 | 20 | 209 | 14 | 242 | E．i0 |
| $358 \times 406 \times 381$ ， | texte | 4＋9．9 | 487.15 | 30.11 | 492 | 152 | 2002 | 4.34 | 2， 20 | 17 | 200 | 5 | 236 | 605 |
| $356 \times 408 \sim 340 \%$ | 3899 | 4084 | 403.0 | 26.6 | 423 | 15.2 | 290．a | 4.70 | 10.9 | ts | 300 | $\cdots$ |  | 8.00 |
| $356 \times 406=897$ ？ | 387， | 3653.8 | 309， | 228 | 36.1 | 152 | 290.2 | 0.47 | 123 | 12 | 500 | 32 | $\pm 3$ | 4．45 |
|  | －gns 1 | $38 \pm 10$ | 394.3 | 柤 4 | 302 | ＋5：2 | 20.2 | 6.54 | 16.3 | 17 | 300 | 46 | 238 | 3.03 |
| $2565368 \times 2029$ | 200：3 | 324．4 | 474．7 | 158 | 570 | 158 | 2000 | 8.34 | 17.9 | 10 |  |  |  |  |
| $298 \times 308 \times 177$ | 1710 | 3882 | 372.8 | 14.4 | 20， 0 | 152 | 290 | 188 | 20.2 | 7 | 100 | 40 | 2.17 | 123 |
| 258 $\times 388 \times 153$ | 1588 | 3020 | 20.5 | 22.3 | 20.7 | 158 | 2992 | 185 | 375 | $\frac{1}{1}$ | 100 | 36 | 2.15 | 14.1 |
| $358 \times 388 \times 125 \times$ | ＋239 | 355.4 | 368.4 | 10．4 |  |  |  |  |  |  | 195 | 3 | 814 | te．0 |
| 206 $\times 305 \times 35$ | 250.8 | 3est | 3223 | 2488 | 4.1 | 15.2 | Suet | 2.65 | 527 | 15 | 158 | 30 | 194 | E．88 |
| $326 \times 395 \times 240$ | 2400 | 3 mg | 318.4 | 23811 | 37．7 | 15\％ | 240， 7 | 1．22 | 70.7 | 14 | 351 | 34 | 1.21 | 7．34 |
| 306 $\times 305 \times 98$ | 198.1 | 2 z | 314.9 | 19.1 | at， 4 | 152 | 2467 | 5 ser | 129 | t | T58 | 40 | 4．57 | 8.40 |
|  | 108 ${ }^{\text {a }}$ | 307， | 3412 | 15：8 |  | 152 | 2057 | 6.28 | 7173 | 10 | ＋58 | 42 | 184 | 11.6 |
| $305 \times 305 \times 137$ | 1988 | 3 mas | 3092 | 13.8 | 21.7 | 15.2 | Vest？ | 7\％ | 1） 3.3 | \＃ | 160： | 33： | 182 | 13.3 |
| $305 \times 305 \times 116$ | 117.9 | 314.4 | 3074 | 12.8 | 187 | 16.2 | 0487 | 822 | 22.5 | 8 | 154 | 31 | 1．11 | 158 |
| $305 \times 1905 \times 01$ | 959 | 307.5 | 305．3 | 39 | 154 | 153 | 346.7 | 997 | 24.9 | 7 | 158 | 3 | 1.73 | 38.5 |
| $254 \times 854 \times 167$ | 1隹， 1 | 200．t | M大き | 粌 | 31.7 | 127 |  |  |  |  | 334 | 45. | 1.58 |  |
| $254 \times 254 \times 130$ | tase | 27 es | 2813 | 14.3 | 253 | 127 | s003 | 5，16 | 13.1 | 10 | 334 | 31 | 45 | 17.7 |
| $254 \times 254 \times 107$ $254 \times 254 \times 99$ | 107.1 980 | 2604 | 288.9 | 12.4 | 20.5 | 12.5 | 20a3 | fiaf | 188 | 8. | 134 | 34 | 158 | 142 |
| 254 $\times 254 \times 90$ | 983 | \％ 60.3 | 2563 | 10.3 | 473 | 12.7 | 2003 | 2.41 | 13.4 |  | 134 | 30 | 150 | 189 |
| $254 \times 254 \times 73$ | 7a1 | 251.1 | 2546 | 18.0 | 142 | 12.7. | 200.3 | 8.90 | 823. | 0 | 134 | 28 | L．49 | 20.4 |
|  |  |  |  |  | 28.5 | 102 | 360.3 | 51.10 | 127 | 3 | 710 | 38 | 1.24 | 14.4 |
| $209 \times 309 \times 7$ | 72.0 | 2158 | zues | 10.0 | 173 | 102 | 190\％ | 597 | 18.1 | 7 | 710 | 28 | 122 | 172 |
| $208 \times 203 \times 60$ | 500 | 2096 | 2058 | 0.4 | 142 | 102 | 1009 | 7298 | 17．1 | 7 | 110 | 2 n | 121 | 20.1 |
| $258 \times 203 \times 52$ $209 \times 208 \times 46$ | 520 | 2082 | 2043 | 79 | 123 | 10.2 | 1008． | 617 | 20.4 | 6 | t10 | 24 | 120 | 23.11 |
| $208 \times 108 \times 46$ | 26.1 | 1052 | 2036 | 73 | 11.0 | 10.2 | 160） | 925 | 293 | 4 | 710 | 22 | t．19 | 2s．1 |
| $352 \times 182 \times 37$ | 37.0 | 151.8 | 154.4 | $\$ 0$ | 11.3 | 75. |  | 0，71 | 155 |  |  |  |  |  |
| $182 \times 162 \times 30$ | 30．0． | 1875 |  | 6.8 | 0.4 | 74 | 1285 | 8．1） | 180 | ， | 84 | 18 | anct | 30.0 |
| $352 \times 159 \times 29$ | 209 | 4 | 152.2 | 89 | 68.8 | 7 f | 1298 | if．a | 213 |  | 84 | 16 | Q 380 |  |

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