2705/302 2709/302 2710/302 STRUCTURES III June/July 2019 Time: 3 hours



THE KENYA NATIONAL EXAMINATIONS COUNCIL

DIPLOMA IN BUILDING TECHNOLOGY DIPLOMA IN ARCHITECTURE

MODULE III

STRUCTURES III

3 hours

INSTRUCTIONS TO CANDIDATES

You should have the following for this examination:
 answer booklet;
 scientific calculator.
This paper consists of EIGHT questions.
Answer any FIVE questions.
Maximum marks for each part of a question are as indicated.
All relevant tables for this examination are provided,
Candidates should answer the questions in English.

This paper consists of 14 printed pages.

Candidates should check the question paper to ascertain that all the pages are printed as indicated and that no questions are missing.

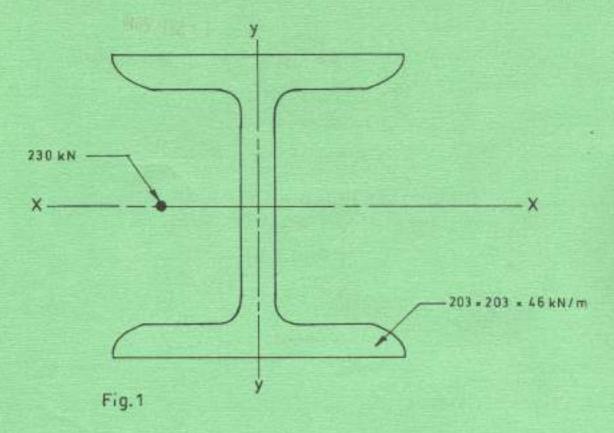
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 A 230 kN reaction from a beam of which a half is due to the imposed loads is supported at the top of a pin-jointed stanchion, 4 m long.

Check if a 203 x 203 x 46 kg/m U.C. in grade S275 steel is satisfactory.

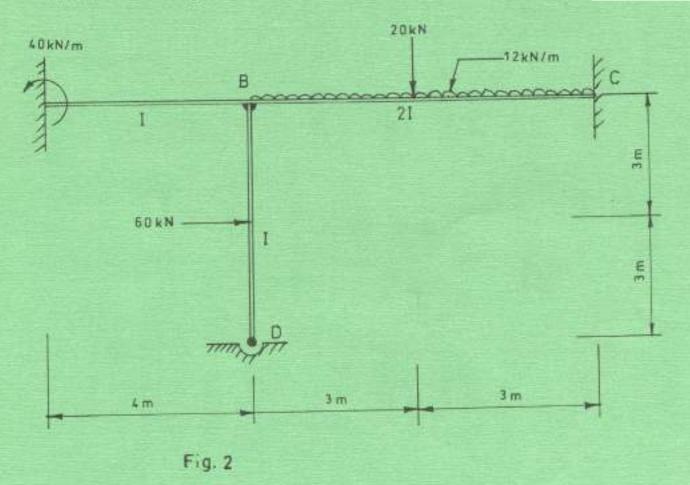
Assume that the beam to stanchion connection is to the web as shown in figure 1.

(20 marks)





Using moment distribution method, analyse the loaded portal frame shown in figure 2 and hence draw the bending moment diagram showing values at critical points.





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- 3, A reinforced concrete suspended slab of a library is supported on universal beams as shown in figure 3. The design loading has been estimated as:
 - Dead loads from slab, finishes, self weight, etc = 6 kN/m²
 - Imposed loads from furniture, books, etc = 4 kN/m²

Determine the suitable section of universal beam for beam B, in grade S275 steel and hence check shear, moment capacity and deflection given that:

- permissible deflection = 1/360 of span.
- E_{steel} = 210 kN/mm² Allowable shear = 0.6 py

(20 marks)

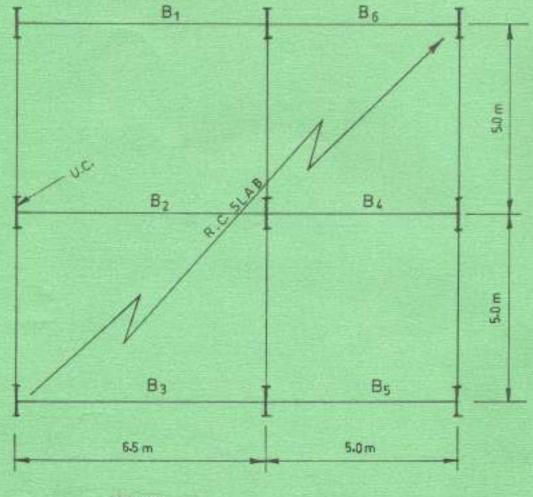
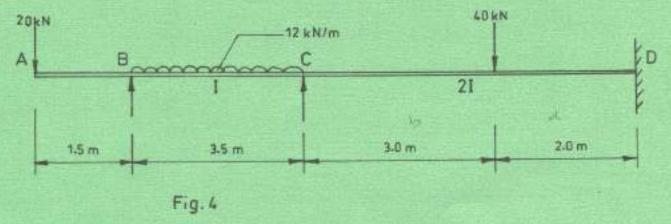


Fig.3



4) Figure 4 shows a loaded continuous beam. Using the three moment theorem, analyze the beam and hence plot the shear force and bending moments diagram indicating values at critical points. (20 marks)



- (a) State two methods of grading structural timber giving one advantage of each.
 (4 marks)
 - (b) Figure 5 shows a loaded timber joist beam. Check the adequacy of the 250 x 100 mm joist in shear, bending and deflection given the following data:

Grade stresses for C18 timber:

- In bending parallel to grain = 5.8 N/mm²
- In shear parallel to grain = 0.67 N/mm²

Permissible deflection = 1/380 of span

Modification factors: $K_3 = 1.25 K_7 = 1.04$ and $K_8 = 1.1$

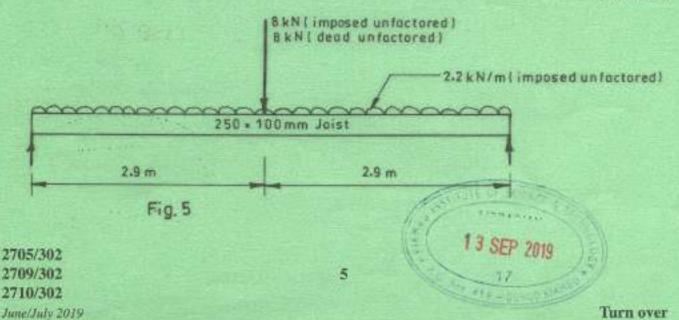
Actual deflection $\delta = \frac{5ul^4}{384 EI} + \frac{Wl^3}{48 EI}$

Where: w = imposed factored load (U.D.L)

W = Imposed factored point loads.

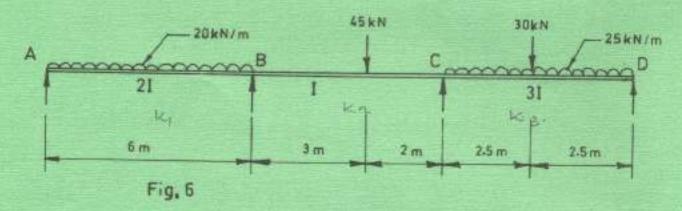
$$E_{mean} = 9100 \text{ N/mm}^2$$

(16 marks)



- 6. (a) State three situations where influence lines can be applied in structures.
 - (b) A girder has a span of 40 m. Two concentrated loads of 18 kN and 25 kN at a fixed distance of 5 m, rolling along it are applied. Find the value of maximum B.M. and S.F. at 10 m, 20 m and 30 m from the left hand end. (17 marks)
- Analyse the loaded beam shown in figure 6 using moment distribution method and hence draw the shear force and bending moment diagrams, indicating values at all critical points.

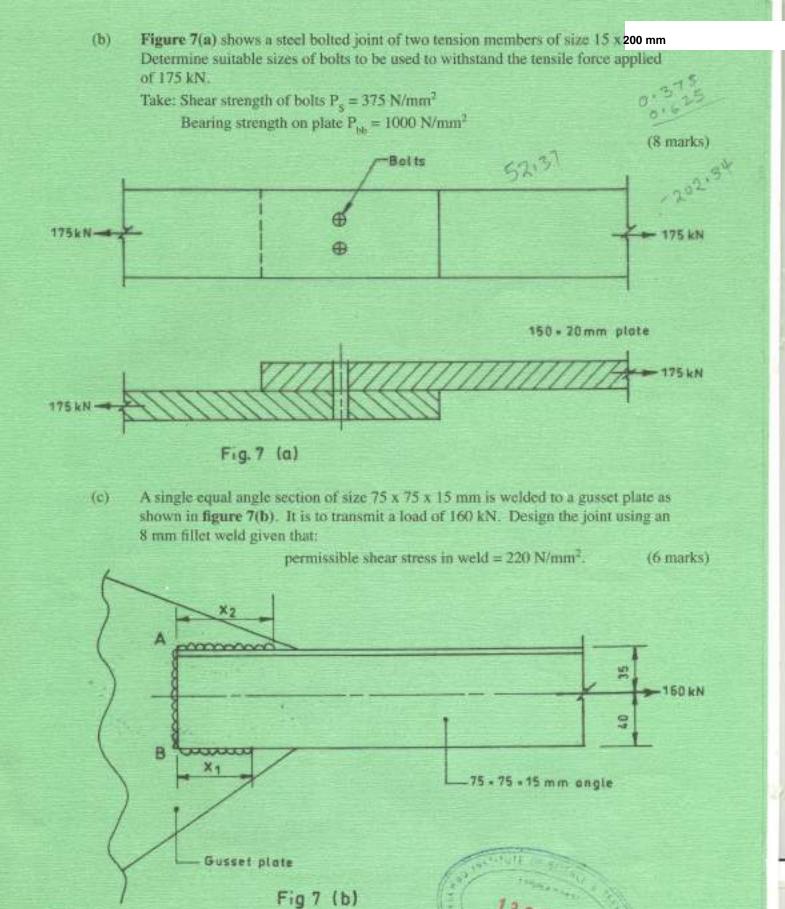
(20 marks)



- 8. (a) Using neat sketches, illustrate the following types of welds:
 - (i) Double 'U' butt weld;
 - (ii) Double 'V' butt weld;
 - (iii) Single 'J' butt weld.

(6 marks)





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Strength of bolts in clearance holes

	Bolt gr	ade (N/mm²)
the Transfer of the	4.6	8.8
Shear strength, p.	160	375
Bearing, strength, psh	460	1035
Tension strength, p.	195	450

Strut table selection

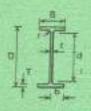
Type of section	Thickness*	Axis	of buckling
		X-X	у-у
Hot-rolled structural hollow section			
Rolled I-section			
Rolled H-section	Up to 40mm	Table 8(a)	Table 8(b)
	Over 40mm	Table 8(b)	

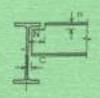
^a For thicknesses between 40 and 50mm the value of pc may be taken as the average of the values for thicknesses up to 40mm and over 40mm

Bar	Numb	Number of bars.													
(mm)	1	2	3	4	5	6	7	8	9	10					
6	28	57	85	113	141	170	198	226	254	283					
8	50	101	151	201	251	302	352	402	452	503					
10	79	157	236	314	393	471	550	628	707	785					
12	113	226	339	452	565	679	792	905	1017	1131					
16	201	402	603	804	1005.	1206	1407	1608	1809	2011					
20	314	628	942	1257	1571	1885	2199	2513	2827	3142					
25	491	982	1473	1963	2454	2945	3436	3927	4418	4909					
32	804	1608	2412	3216	4021	4825	5629	6433	7237	8042					
40	1256	2513	3769	5026	6283	7539	8796	10050	11310	12570					



UNIVERSAL BEAMS





DIMENSIONS

Section Designation	Mass	Depth	Width	Thi	CHINE	Root Radius	Depth		os for Suckling		anoise prilian	for	Surfa	on Arms
	Metro	Section	Section	Wet	Flange		Filets	Flange	10000	End	N N	out	Par Metre	Per Tonne
	kg/m	inm.	B mm	1	T mm	rom	d mm	ьт	run.	C mm	M	n	m	m²
457 × 191 × 94 457 × 191 × 86	89.3	487.2 483.4	192.8	11.4 10.5	19.6	10.2	407.8 407.3	4.92 5.42	35.8	* 7	102	30	1,67	19.9
457 × 191 × 84 457 × 191 × 74 457 × 191 × 67	74.3	450.0 457.0 453.4	191,3 190,4 190,0	9.0 9.0 8.5	16.0 14.5 12.7	10.2	407.6 407.6	5,08 6,57 7,48	41.2 45.3 48.0	7 7 9	102 102 102	26 26 24	1.85 1.64 1.63	20.1 22.1 24.3
457 × 182 × 10 467 × 162 × 74		465.8 462.0	155.3 154.4	10.5	18.9 17.0	10.2	607.5 407.5	4.11	38.8 42.5	7	84	30	1.51 1.50	18.4
467 × 152 × 67 467 × 152 × 80 457 × 152 × 50	59.8	458.0 454.6 449.8	153.8 152.9 152.4	9.0 8.1 7.8	15.0	10.2 10.2	407.8 407.6 407.6	5.13 5.75 6.99	45.3 50.3 53.8	7	84 84	26 24 22	1,50	22.3
406 × 178 × 74	74.2	412.8	179.5	9.5	10.0	10.2	300.4	5.81	37.9	1	96	28	1,51	28.2
406 × 178 × 67 406 × 178 × 60 405 × 178 × 54	87.1 80.1 54.1	408.4 408.4 402.6	1778.8 177.9 177.7	7.8 7.7	14.3 12.8 10.0	10.2 10.2	360.4 388.4 360.4	5.95 5.95	41.0 45.8 46.8	6 6	96 96 96	26 24 22	1,50 1,49 1,48	22.3 24.B 27.4
406 × 140 × 48 406 × 140 × 19	48.0 30.0	403.2 396.0	142.2 141.8	0.8 6.4	11.2	10,2	360.4 360.4	8.35 8.34	50.0	5	78 78	22	1.34	29.2
955 × 171 × 67 196 × 171 × 57	67.1 57.0	363.4 358.0	173.2 172.2	9.1	15.7	10.2	311.6	5.52	34.2 36.5	7 6	94	26 24	1.30	20.0
158 × 171 × 51 156 × 171 × 48	81.0 45.0	385.0	171.5 171.1	7.4	11.5 9.7	10.2	311.6	7.46 8.82	42.1 44.5	8	3.3	20 20	1.36 1.36	36.7 30.1
56 × 127 × 39 56 × 127 × 03	39.1	363,4 349.0	125.0 125.4	6.6	10.7 8.5	10.2	311.6	5.88 7.38	47.2 51.9	5 5	22	222	1,518 1,17	30.E 35.4
05 × 165 × 54 05 × 165 × 40 05 × 165 × 40	54.0 45.3 40.3	310,4 308,8 309,4	188.9 185.7 185.0	7.9 8.7 8.0	13.7 11.8 10.2	9.8 5.9 8.9	265.2 265.2 265.2	8.09 7.02 8.09	33.8 39.6 44.2	5 5	90 90	24 22 20	1.26 1.25 1.24	23.3 27.1 30.8
05 × 127 × 48 05 × 127 × 42 05 × 127 × 37	48.1 41.9 37.0	311.0 307.2 304.4	125.0 124.0 123.4	9.0 8.0 7.1	14.0 12.1 10.7	8.9 3.0 8.0	265.2 295.2 285.2	4.47 5.14 5.77	29.5 33.1 37.4	7 0 0	70 70 70	24 22 20	1.09	22.7 25.8 29.0
05 × 102 × 33 05 × 102 × 28 05 × 102 × 25	32.8 38.2 24.8	312.7 308.7 305.1	302.4 301.8 101.6	5.6 6.0 5.9	10.B 8.8 7.0	7.6 7.6 7.6	275.0 275.0 275.0	4.74 5.78 7.25	41.8 48.0 47.6	1 1	58 58 58	26 18	1.01	30.8 35.4 40.0
54 × 148 × 43 54 × 146 × 37 58 × 146 × 31	43.0 37.0 31.1	259.6 256.0 251.4	147.3 146.4	7.2 6.3 6.0	12.7 10.9 2.6	7.8 7.6 7.6	219.0 219.0 219.0	5.80 6.72 6.69	39.6 34.8 34.5	6 5 5	82 82	22 20	1.08	25.1 29.0 34.2
54 × 102 × 28 54 × 102 × 25 54 × 102 × 25	38.3 25.2 22.0	287.2 284.0	102.2	6.3 6.0 5.7	10.01	7.d 7.0	225.2	5.11 6.07	35.7	3 5	58 58	18 1	1.904	31.9
0 × 133 × 30 0 × 133 × 35	30.0 25.1	2068	133.9	6.4 5.7	0.6 7.8	7.6 7.8	225.2 172.4 172.4	7.47 6.97 8.54	29.5 29.9 30.2	5 5	74 74	18 (1829	10.0 30.4
15 × 100 × 211	23.1	200.2	101-8	5.4	6.0	7.0	169.4	Control of	21.4	5	80		Out of	34.2
8 × 102 × 18	19.0	177.8	1012	6.8	7.51	7.6	148.8	6,41	30,6	4.	00	10 0	738	30.6
2 K 85 K 16	19.0	152.4	99.7	1,5	7.7	7.8	121.8	5.76	27.1	4	54	1E 0	1638	30.0
7 × 76 × 15	ma	107,0	76.0	10	7.8	7.0	90.0	5.00	24.1	#	46	in o	1537	41.3

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Table 8(a): Compressive strength, p_e (N/mm³) for struts

		_					_				
PY	225	245	255	265	275	PY	225	245	255	265	275
A S						7	400				
15	225	245	255	265	275	96	133	140	143	146	148
20	224	243	253	263	272	98	130	137	139	142	145
25	220	239	248	258	267	100	127	133	136	138	141
30	215	234	243	253	262	102	124	130	132	135	137
35	211	229	238	247	256	104	122	127	129	131	133
40	207	224	233	241	250	106	119	124	126	128	130
42	205	222	231	239	248	108	116	121	123	125	126
44	203	220	228	237	245	110	113	118	120	121	123
46	201	218	226	234	242	112	111	115	117	118	120
48	199	215	223	231	239	114	108	112	114	115	117
50	197	213	221	229	297	116	105	109	111	112	114
52	195	210	218	226	234	118	103	106	108	109	111
54	192	208	215	223	230	120	100	104	105	107	108
56	190	205	213	220	227	122	98	101	103	104	105
58	188	202	210	217	224	124	96	99	100	101	102
60	185	200	207	214	221	126	94	96	97	99	100
62	183	197	204	210	217	128	91	94	95	96	97
64	180	194	200	207	213	130	89	92	93	94	95
66	178	191	197	203	210	135	84	86	87	88	89
68	175	188	194	200	206	140	79	81	82	83	84
70	172	185	190	196	202	145	75	77	78	78	79
72	169	181	187	193	198	150	71	72	73	74	74
74	167	178	183	189	194	155	67	69	69	70	70
76	164	175	180	185	190	160	64	65	66	66	66
78	161	171	176	181	186	165	60	61	62	63	63
80	158	168	172	177	181	170	57	58	59	59	60
82	155	164	169	173	177	175	55	56	56	56	57
84	152	161	165	169	173	180	52	53	53	54	54
85	149	157	161	165	169	185	49	50	51	51	51
88	146	154	158	161	165	190	47	48	48	48	49
90	143	150	154	157	161	195	45	46	46	46	47
92	139	147	150	153	156	200	43	44	44	44	44
94	136	143	147	150	152		-			-0.5	
-	No. of Concession,	- Control	STATE OF THE PARTY OF	salarahed fil	- Indeed						_



Table 8(b): Compressive strength, pc (N/mm²) for struts

-	-	-			100	A STATE OF THE PARTY OF THE PAR	ili	-	and and		
PY	225	245	255	265	275	Py	225	245	255	265	275
1	-					3			74		-
15	225	245	255	265	275	96	118	124	127	129	132
20	224	242	252	261	271	98	115	121	123	126	129
25	217	235	245	254	263	100	112	118	120	123	125
30	211	228	237	246	255	102	110	115	118	120	122
35	204	221	230	238	247	104	107	112	115	117	119
40	198	214	222	230	238	106	105	110	112	114	116
42	195	211	219	227	235	108	102	107	109	111	113
44	193	208	216	224	231	110	100	104	106	108	110
46	190	205	213	220	228	112	98	102	104	106	107
48	187	202	209	217	224	114	96	99	101	103	105
50	184	199	206	213	220	116	93	97	99	101	102
52	181	196	203	210	21.7	118	91	95	9.6	98	100
54	179	193	199	206	213	120	89	93	94	96	97
56	176	189	196	202	209	122	87	91	92	93	95
58	173	186	192	199	205	124	85	88	90	91	92
60	170	183	189	195	201	126	83	86	88	89	90
62	167	179	185	191	197	128	82	84	86	87	88
64	164	176	182	188	193	130	80	82	84	85	86
66	161	173	178	184	189	135	75	78	79	80	81
68	158	169	175	180	185	140	71	74	75	76	76
70	155	166	171	176	1.81	145	68	70	70	71	72
72	152	163	168	172	177	1.50	64	66	67	68	68
7.4	149	159	164	169	173	155	61	63	63	64	65
76	146	156	160	165	169	160	58	59	60	61	61
78	143	152	157	161	165	165	55	56	57	58	58
80	140	149	153	157	161	170	52	54	54	55	55
82	137	146	150	154	157	175	50	51	52	52	53
84	134	142	146	150	154	180	48	49	49	50	50
86	132	139	143	146	150	185	46	46	47	47	48
88	129	136	139	143	146	190	43	44	45	45	46
90	126	133	136	139	142	195	42	42	43	43	43
92	123	130	133	136	139	200	40	41	41	41	42
94	120	127	130	133	135						14
	-	-	_		-						



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PROPERTIES

Designation		Araa Araa		ladius Byratlar	Me	destic odulus		auto dulus	Buckling Parameter	Torsional Index	Warping Constant	Torcional Comment	Am
	Axia.	Ances	Atti		All IIII Comm	A STATE OF THE PARTY OF THE PAR	Asm	Assign			I WAR	- I	Sec
	om,	Sam,	(III		No.	om ₃	OLD ₂	CALS.	-		H dim*	om'	A con
386 × 406 × 634 #	275000					4830	14200	7110	0.840	5.46	70.4	- Interes	Section 1
355 × 406 × 531 #	227/000		1,100		9960	20060	12100		0.841	8.05	38.8	13700	30
256 × 406 × 467 #	183000		17,4		8260		10000		0.639	0.05	24.3	9940	70
156 × 406 × 383 # 156 × 406 × 340 #	147000	55400	177		7000	2723	8220	4150	9.837	7.87	18.9	5810	599
56 × 406 × 267 a	123000	66900	16.8		6030	2330	7000	3540	0.836	1.84	15.5	3500	50
	99900	-38700	16.5		50en	1940	SHIO	11950	0.834	10.2	12.3	2940	43
56 × 406 × 235 #	79100	31000	16.8	10.2	4150	1570	1600	2380	0.835	12.0	0.54	1440 812	36
58 × 368 × 202 a	96300	23700	16.7	9.60	3540	1280	3970	1820	0.848	1000			100
58 × 308 × 177.9	57100	20500	15.9		2100	1100	3460	1670	0.843	13.4	7.10	058	25
58 × 368 × 153 #	48500	17800	15.8	IF.40	0880	948	2970	1440		15.0	6.09	381	225
58 × 388 × 129 ø	40300	14600	15.8	9,40	2260	793	2480	1200	0.845	17.0	E.11 4.18	251	184
15 × 305 × 283	78000	24800	14.8	8.27	4320	4 000		1000				100	-10
35 × 305 × 240	64290	20300	14.5	8.15	3840	1530	5110	2340	0.858	7.55	8.35	2000	360
16 × 305 × 198	50900	18500	14.2	8,04	-3000	1040	4850	#95D	0.054	B.74	5.00	1270	306
25 × 305 × 150	38800	12600	19.3	7.90	2370	808	3440	1590	0.004	10.2	3.88	734	255
5 × 305 ± 137	20900	10700	12.7	7.83	2050	692	2580	1230	0.862	TR.5	2.87	378	2891
5 × 305 × 118	27700	9080	13.6	7.77	1760	589	2300	1050	0.852	16,1	2.39	249	174
5 × 305 × 97	82000	7310	12.4	7.59	1450	479	1960	895	0.851	16.2	1.98	101	150
				10000	1100	412	1590	728	0.862	10.0	14	91.2	123
4 × 254 × 187 4 × 254 × 102	30000	1807G 7530	H.B.	6.81	2000	244	2420	1140	0.851	8.50	1.63	626	213
4 × 254 × 107	17500	5630	11.8	6.09	1630	576	1870	878	0.850	10.3	1.19	219	168
4 × 254 × 89	14300	CONTRACTOR OF	11.3	8.59	1310	450	5480	697	0.849	124	0.898	172	136
4 × 254 × 73	11400		11.2	6.55	1100	379	1220	574	0.851	14.5	0.717	102	
THE PERSON AND ADDRESS OF THE PERSON ADDRESS OF THE PERSON AND ADDRESS OF THE PERSON ADDRE	trapp	3910	17.1	0.48	989	307	292	465	0.849	17.0	0.562	57.8	99.1
3 × 203 × 86	9450		9.28	5.34	860	299	977	456	0.848	100		A STATE OF	
3 × 203 × 71		2540	B.T.B	0.00	706	246		374		10.2	0.318	137	T10
3 × 203 × 60	ятао	2070		8.20	584	TO STORY AND ADDRESS OF		305	0.853	11.9	0.250		90,4
1×203 x 52				5.18	510	77777		284	0.846	14.1	0,197		75.4
× 203 × 48	4670			5.15	450		THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	231	0.846	15.8	0.167		68.3
× 152 × 37	2210	708 (Lis	3.87	979	20.5	1000	7710	Annual Control		MH COLD III	-	201
A CONTRACTOR OF THE PARTY OF TH	COCCUSION CONTRACTOR			1.83				140	0.840		0.00399	19.2	67.1
	1250			1.70	202			112	0.848		A 14 A 15 A 16		38.3
CONCESSION OF THE PARTY OF THE	American Police	THE REAL PROPERTY.	255	B+ 0 M	164	52.6	182	0.2	0.840			277774	29.2

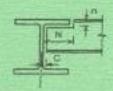


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DIMENSIONS

Section Designation	Atass per	Depth	Wan	This	zkneaz	Rect Radius	Depth -	Local B		Dimens	plans t	mr.	Surta	de Are
	Metra	Bection	Section	Web	Flange		Flats	Plange	White	first Clearance	740	rita Pi	Hetre Metre	Per
	lug/m	D mm	th mm	nm.	T mm	imm	of norm	ыт	dt	C	N	mm	ma.	mi
156 × 406 × 834 #	633.0	474.5	424.0	47.6	77.0	152	290.2	2.75	8.10	26	200	the	2.52	3.9
156 × 406 × 551 #	551.0	455,6	418.5	42.1	67.5	152	290.Z	3.10	6.89	23	200	04	2,47	4.4
55 × 405 × 467 #	467.0	436.6	412.2	35.8	38.0	15,2	290.2	3.55	8.77	20	200	74	2.42	5.1
56 × 406 × 383 # 55 × 406 × 340 #	090.0	419.0 405.4	407.0	30.8	49.2	15.2	290.2	4.34	8,40	17	200	95	2.38	6.0
56 × 406 × 287 #	287.1	383.6	403.0 309.0	28.6	42.9 36.5	15.2	290.2	6.47	10.9	15	200	60	2.30	6.0
56 × 406 × 235 #	235.1	381.0	394.8	18.4	30.2	15.2	530.5	0.54	15.8	11	300	46	2.28	9.0
56 × 368 × 202 A	201.0	374.8	574.7	16.5	27.0	15.2	290.5	8.04	17.6	10	100	44	8.10	10.
08 × 388 × 177 #	177.0	388.2	372.6	14.4	23.0	18.2	290.E	7,83	30.2	9	100	40	2.17	12.
56 × 368 × 153 #	158.8	0.590	370.5	12.3	20.7	15.2	290.2	8.95	83.6		190	36	2.16	14:
96 × 368 × 129 ¥	129.0	355.0	368.0	10.4	17.5	15.2	290,2	10.50	27.9	7	195	34	2.54	16.
65 × 305 × 283	282.9	365.3	322.2	26.8	44.1	15.2	240.7	0.65	5.21	15	158	80	1.94	6.8
05 × 305 × 240 05 × 305 × 198	198.1	352.5	318.4	23.0	37.7	15.2	240,7	A.22	10,7	14	758	54	1.91	7.B
25 × 305 × 158	158.1	327.1	311.2	15.8	25.0	15.2	246.7	5.01	12.9	12	158	40	1,87	9,4
25 × 305 × 157	136.0	320.5	309.2	13.8	21.7	15.2	246.7	7.12.	17.0	8	158	38	1.82	13.
35 x 305 x 118	117.9	514.5	307.4	12.0	18.7	16.2	.046.7	8.22	20.5	8	152	34	1.81	151
05 × 305 × 97	96.9	307.9	305.3	9.9	15.4	15.2	246.7	9,91	24.9	7	158	32	1,79	18.
94 × 254 × 167	167.1	289.1	255.2	19.2	31.7	12.7	200.5	4.18	10.4	12	134	46	1,58	9.45
4 x 254 x 132	132.0	276.3	281,3	18.3	25.5	12.7	200.3	5,18	13.1	10	104	38	1.55	11.5
4 × 254 × 107	107.1	206.7	258.0	12.8	20.5	12.7	500.3	fl.DF	15.6	8	134	34	1.52	143
4 x 254 x 99 4 x 254 x 73	98.0 73.1	250,3	258.3	10.3	17.3	12.7	200.3	7.41	10,4	7	134	30	1.50	18.0
4 x 604 x (3	FG.1	254.1	254.6	8.6	142	12.7	200.3	8.96	23.3	6	104	28	1.40	50.4
0 × 203 × 86 0 × 200 × 71	71.0	222.2		12.7	20.5	10.2	160-8	5.10	12.7	8	110	32	1.24	184
0 × 203 × 80	80.0	209.6	205.8	0.4	17.3	10.2	190.8	5.97 7.25	18.1	7	110	28	1,22	17.2
0 × 203 × 52	52.0	208.2	204.3	7.9	12.5	10.2	100.6	8.17	20.4	6	110	24	121	23.0
3 × 203 × 46	46.1	300.5	203.6	72	11.0	10.2	160.8		22.3		110	222	1.19	25.8
2 × 152 × 37	37.0	181.8	154.4	8.0	11.5	7.6	123,6	0.71	15.5		64	20	0.912	24.7
2 × 152 × 30	30.0	157.6		5.5	9.4	78	123.8		18.0		84		0.001	10.0
2 x 152 x 23	23.0	189.4	152.2	5.8	6.8	7.6	123.6		21.2		84	16	0.880	38.7

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